

## Nematic effects and strain coupling in entangled polymer melts under strong flow

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We use small-angle neutron scattering (SANS) to study labeled short chains with and without the influence of an entangled and highly stretched surrounding environment of longer chains. We find unequivocal evidence of nematic effects as the blend chains in steady state flow are stretched a factor  $\sim 1.5$  more from the presence of the long chain nematic field. In the pure melt we confirm that the nonaffine mean-field result  $\nu = 0.5$  for the strain coupling is still valid for very fast flows, while in the nematic system our analysis predicts an increased coupling constant. We provide a structural explanation for the two first regimes of the nonlinear relaxation, particularly a transition regime where the long chains are relaxing in a sea of reptating short chains.

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### I. INTRODUCTION

Filament stretching rheometry (FSR) allows large deformation up to Hencky strain 7 (stretch ratio 1000) with accurate constant stretch rates and subsequently keeping the large deformation state during relaxation of the sample. These unique features of the FSR therefore open up new investigations in large strain polymer dynamics [1,2]. Despite the recognized success of the classical Doi-Edwards tube model [3] and its later modified manifestations [4], the nonlinear viscoelastic behavior of entangled polymer chains in fast flows still possesses a challenge, and there is currently no full theoretical description of the underlying physics in such systems. One novel parameter in the tube model, proposed very recently in both simulations [5,6] and experiments [7,8], is the anisotropic friction due to nematic interactions between polymer-polymer (long chain-long chain) and polymer-oligomer (long chain-short chain). However, the possible changes of molecular configurations resulting from such nematic interactions, which may be seen in SANS, have not yet been systematically investigated. Here we push the idea of an entangled polymer system diluted by shorter chains into the regime of a bidisperse melt of long and short entangled chains and flip the viewpoint by focusing on the short chain behavior and how these are influenced by the presence of a highly entangled and stretched surrounding environment of longer chains. We exploit the power of FSR to perform true stress relaxation experiments after steady state flow and combine these with SANS experiments to obtain unique structural information on the short chain conformations during relaxation with and without the influence of the stretched long chain environment.

### II. EXPERIMENTAL

We investigate two systems: a pure melt of short polystyrene (95 kg/mol) chains and a bidisperse melt composed of a 50/50 wt mixture of short and long (545 kg/mol) polystyrene

chains. Note that both chain populations are entangled with the number of entanglements per chain  $Z_L \approx 41$  and  $Z_S \approx 7$  for the long and short chains, respectively [9]. In both systems a fraction of the short chains are deuterated and thus allow for direct comparison of the short chain relaxation in these two scenarios. We label these two sample series Short-in-Short (SiS) and Short-in-Long (SiL), respectively. Synthesis and chromatography of the monodisperse polystyrenes, PS-545k and PS-95k, used in this work have already been described along with characterizations of both shear and extensional rheology [9,10]. The main characteristics of the sample constituents are summarized in Table I. The samples were stretched with the VADER 1000, Rheo Filament ApS, a commercially available filament stretching rheometer. As shown in Ref. [9] extensional steady state flow conditions are established beyond a Hencky strain of  $\epsilon = 3$ , and a total of five strain rates were rheologically tested probing different flow regions separated by the time constants of the constituent chains. Here we focus our attention to  $\epsilon = 3$  and to the highest strain rate investigated,  $\dot{\epsilon} = 0.1 \text{ s}^{-1}$ . We note that we also find nematic effects at lower strain rates, which will be presented elsewhere. The details of the stretching experiments are given in Ref. [9]. However, for the SANS experiments it is vital to quench the samples fast enough to trap the relevant molecular configurations. Stretching is performed at  $130^\circ\text{C}$ , and our procedure results in a cooling rate of ca. 10 K/s, ensuring that within  $\sim 3 \text{ s}$  the sample is below its glass transition temperature [11]. This time is much smaller than the Rouse time of the short polymer chains ( $\sim 20 \text{ s}$ ), so we are confident that the initial molecular configuration survives. This is confirmed by scattering experiments on samples quenched at a lower temperature ( $125^\circ\text{C}$ , but at the same Weissenberg number), which within experimental error are identical to the  $130^\circ\text{C}$  results. Figure 1 shows the stress relaxation data for the SiL and SiS samples normalized by the first value of the stress decay  $\sigma(t=0)$  plotted against time where  $t=0$  is the steady state and the start of the relaxation part of the experiment. The red arrows highlight the times at which a quenching was performed, and thus six different stages of the relaxation process have been investigated. In the figure the Rouse and

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TABLE I. The weight-average molecular weight  $\bar{M}_w$ , the polydispersity index PDI, and the weight fractions of the polymers used in the samples SiL (Short-in-Long) and SiS (Short-in-Short).

Components	PS-545k	PS-95k	D-PS-86k	D-PS-80k
$\bar{M}_w$ [g/mol]	545 000	95 100	86 300	80 000
PDI	1.12	1.07	1.02	1.02
Sample SiL (wt%)	50	40	10	0
Sample SiS (wt%)	0	90	0	10

reptation time of the monodisperse linear short components are indicated. In Ref. [9] the rheology data of the blend is separated into three domains approximately defined in the following time intervals: a fast regime (0–20 s), a transition regime (20–700 s), and a slow regime for times longer than 700 s. It is hypothesized that the fast regime is dominated by fast stretch relaxation (note that the blend initially relaxes faster than the pure short chain melt) and the slow regime by long chain relaxation in a sea of essentially relaxed short chains. The transition regime is speculated to originate from retraction of long chains in a sea of reptating short chains. Here we aim to clarify the structural origin of this rheological behavior using SANS.

SANS originate from different beam lines. First experiments were performed at the SANS-1 instrument at the Swiss Spallation Neutron Source (SINQ) and the second at the Quokka beam line at ANSTO, Australia. In both cases three overlapping settings covered a full  $q$  range from  $5 \times 10^{-3} \text{ \AA}^{-1}$  to  $0.25 \text{ \AA}^{-1}$ . We followed standard data reduction procedures, i.e., correcting for detector efficiency using incoherent water scattering, and subtracting background scattering, which is dominated by the incoherent scattering from polystyrene and measured in a polystyrene sample with no deuterated chains.

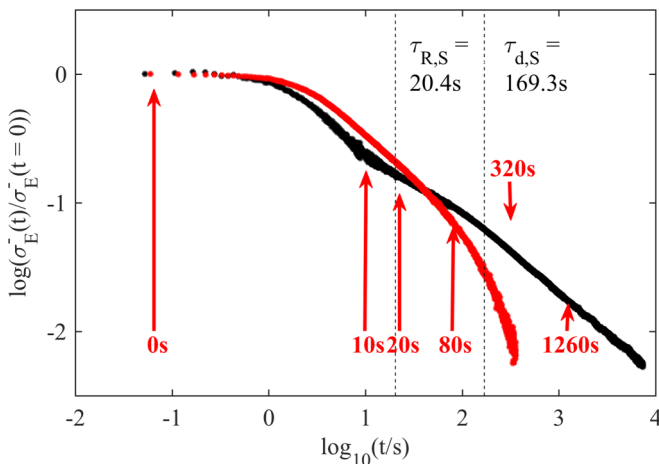


FIG. 1. Tensile stress  $\sigma_E^-$  of the SiL (black) and SiS (red) samples at  $130^\circ\text{C}$  after cessation of fast uniaxial elongational flow at Hencky strain  $\epsilon = 3$  and strain rate  $\dot{\epsilon} = 0.1\text{s}^{-1}$ . Dashed vertical lines indicate the short chain Rouse and reptation time. Red arrows indicate times where a quenched sample was produced for scattering studies.

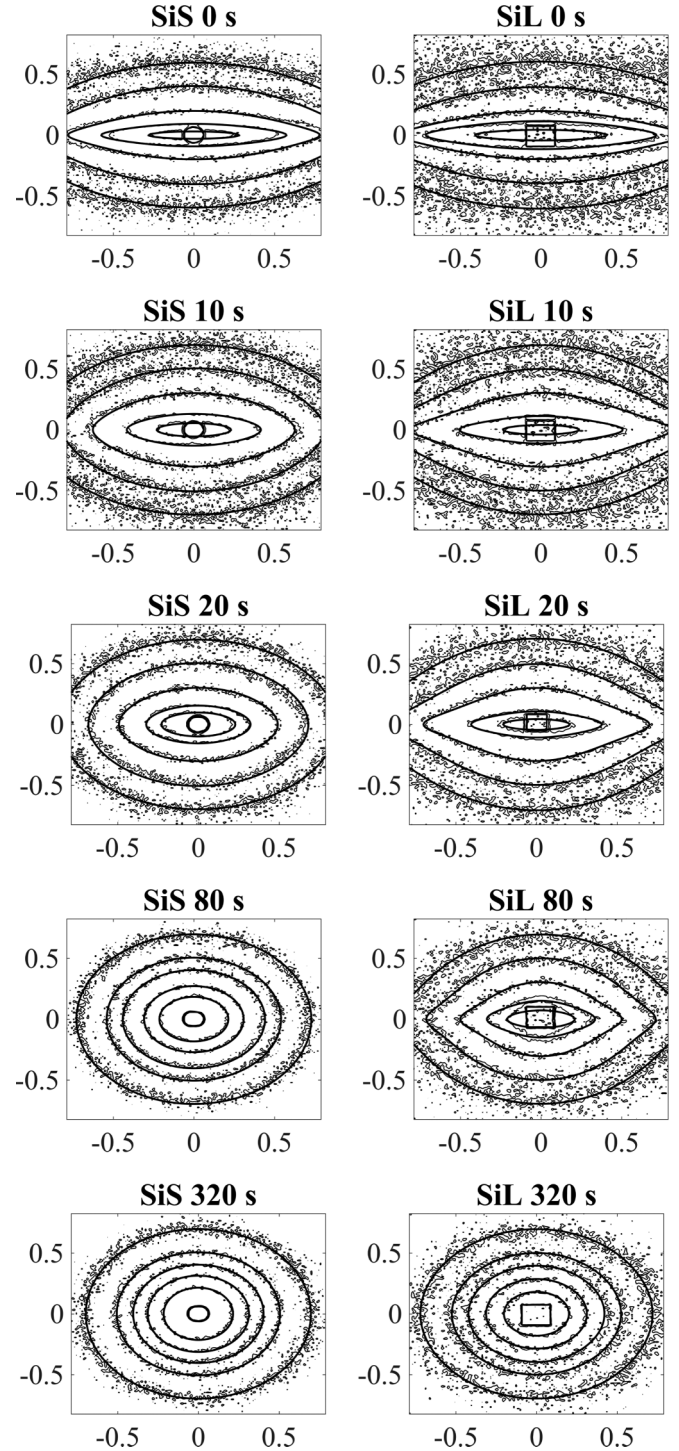


FIG. 2. Two-dimensional scattering data and accompanying fits for both sample series. We omit the totally relaxed 1260 s data. Units are in  $\text{nm}^{-1}$ . (Left) SiS sample for times 0, 10, 20, 80, and 320 s. (Right) Same for the SiL sample.

### III. MODELING

Here we focus on the central setting for 2D fitting since the relevant length scales are best represented here. Our anisotropic SANS data can be modeled using the Warner-Edwards (WE) model [12] for the SiS sample and the modified WE model with dangling ends (DE model) [13], which we

find to be directly applicable for the SiL system without the complications arising from chain scission, etc., present in a crosslinked system [14–16]. As shown below the SiL data show distinct lozenge patterns, while the SiS samples do not. The appearance of lozenges requires some chains to remain stretched while others relax; i.e., it requires an effective network, in the form either of a crosslinked system as was the subject in the original DE papers [13,14] or of a sufficiently long-lived entanglement network which is thus the case in the SiL sample but, according to our data, not in the SiS sample.

In the DE model each chain is described as having two dangling ends, each a fraction  $f$  of the total chain. The total scattering function is a combination of terms from the isotropic dangling ends described by Gaussian chain statistics and the central stretched portion described by the WE model. Thus, the DE model reduces to the WE model for  $f = 0$ . In both models the tube diameter is given by  $d_\mu = d_0 \lambda_\mu^\nu$  with  $\lambda_\mu$  being the microscopic strain ratio in direction  $\mu$  ( $\mu = x, y, z$ ) where  $z$  is the stretch direction,  $d_0$  the tube diameter of the relaxed melt, and  $\nu$  a parameter allowing for anisotropic strain coupling of the tube potential. Assuming incompressibility, the perpendicular strain ratios are related to  $\lambda_z$  as  $\lambda_x = \lambda_y = 1/\sqrt{\lambda_z}$ . It is important to recognize that the microscopic and macroscopic strain ratios are not necessarily the same [17], and a number of models have attempted to relate the two theoretically [18]. In particular, the value of the strain coupling has been a topic of discussion for some time [13,19,20] but for moderate strain ratios has been clearly demonstrated experimentally to be nonaffine with  $\nu = 0.5$  [20] confirming various theoretical predictions [21,22]. However, it is unclear if this scaling also applies for the much higher strain ratio described here and how the exponent would change in a system influenced by nematic effects. Further, it is not clear how  $\nu$  and (the effective microscopic)  $\lambda_z$  behaves as the system relaxes. In our experiments, the macroscopic strain ratio experienced in the filament plane of observation at  $t = 0$  for the employed Hencky strain is  $\lambda_{z,\text{mac}} = \exp(3) \approx 20$ . Notice that this is considerably higher than any previously reported elongation ratio in SANS-based structural studies of fully labeled chains, to our knowledge a factor of 4–5 higher. We present fits where we allow both  $\nu$  and  $\lambda_z$  to vary but impose constraints by the following strategy: Each consecutive fit uses the fit of the previous time point as lower and upper bounds with the following assumptions: the fraction of dangling ends is monotonically increasing in time and approaches  $f = 0.5$  for long times, the strain coupling will be isotropic in the long time

limit ( $\nu = 0$ ), and finally the effective strain felt by the short chains will be monotonically decreasing as the system relaxes. We note that we find it impossible to fit the  $t = 0$  data assuming affine or isotropic microscopic deformations ( $\nu = 1$  or  $\nu = 0$ ) with reasonable physical parameters. In our analysis we fix  $R_g = 7.82$  nm, the value obtained from an isotropic Debye fit to the fully relaxed sample and  $d_0 = 7.51$  nm, calculated from  $R_g^2 = d_0^2 Z_S/6$ . The fits are done using custom-made Matlab code minimizing the residuals in a least-square sense. The actual fit parameters are listed in Table II, and the 2D fits are shown in Fig. 2. The fitting gives the presented evolution of the main fit parameters shown in Fig. 3 with suitable normalizations.

#### IV. RESULTS

From a simple visual inspection of the 2D data in Fig. 2 it is clear that the short chain relaxation is affected by the presence of the long chains, immediately indicating a nematic effect of the long chains. It has previously been demonstrated with infrared dichroism and NMR in similar systems of long and short blends that the local orientational order of the two chains is identical [23,24], and thus we can ascribe any difference in the principal axis parameters as originating directly from a difference of the short chain stretching. Let us first focus on the initial quench in the steady state. The effective extension ratio is  $\lambda_{z,\text{eff}} = d_z/d_0 = \lambda_z^\nu$ , which we can compare to either the fully oriented, but unstretched chain or the fully stretched chain via the end-to-end vector. The ratios in those two cases are  $Z_S d_0/\sqrt{6} R_g \sim 2.75$  and  $N_k b/\sqrt{6} R_g \sim 10.5$ , respectively [25]. The numbers for the SiS and SiL samples are  $\lambda_{z,\text{eff}}^{\text{SiS}} = 16.21^{0.52} = 4.2$  and  $\lambda_{z,\text{eff}}^{\text{SiL}} = 21.72^{0.61} = 6.54$ . Thus, the SiS chains are stretched a factor 1.5 relative to the fully oriented chain or 40% of the fully extended chain. The SiL chains are stretched a factor 2.4 relative to the fully oriented chain or ca. 60% of the fully extended chain. So relative to the SiS sample, i.e., without the nematic field of the long chains, the short chains in the blend are stretched an extra  $\sim 50\%$ . Thus, the combined effect of the flow and the nematic field of the oriented long chains not only orients and stretches the short chains but increases the experienced stretch. In fact, the SiL fit predicts a microscopic  $\lambda_z$  value higher than the macroscopic strain ratio. These findings can be rationalized only if direct nematic interactions exist between the chains.

As the chains start to relax it becomes clear that the behavior in the two scenarios is also quite different. If we focus on the relaxation of the SiS sample first, the fit for  $t = 0$  basically

TABLE II. Parameters from the WE/DE-model fits.

Time	SiS $\lambda_z$	$\nu$	SiL $f$	$\lambda_z$	$\nu$
0	$16.21 \pm 1.8$	$0.52 \pm 0.01$	$0 \pm 0.01$	$21.72 \pm 4.5$	$0.61 \pm 0.02$
10	$5.59 \pm 0.39$	$0.45 \pm 0.02$	$0.16 \pm 0.02$	$19.55 \pm 4.8$	$0.6 \pm 0.02$
20	$2.82 \pm 0.22$	$0.43 \pm 0.05$	$0.21 \pm 0.02$	$17.59 \pm 5.9$	$0.59 \pm 0.02$
80	$1.22 \pm 0.13$	$0.36 \pm 0.04$	$0.33 \pm 0.04$	$17.36 \pm 5.2$	$0.52 \pm 0.06$
320	$1 \pm 0.1$	$0.09 \pm 0.01$	$0.47 \pm 0.05$	$15.61 \pm 4.08$	$0.48 \pm 0.05$
1260	$1 \pm 0.1$	$0.01 \pm 0.01$	$0.48 \pm 0.02$	$2.59 \pm 0.88$	$0 \pm 0.01$



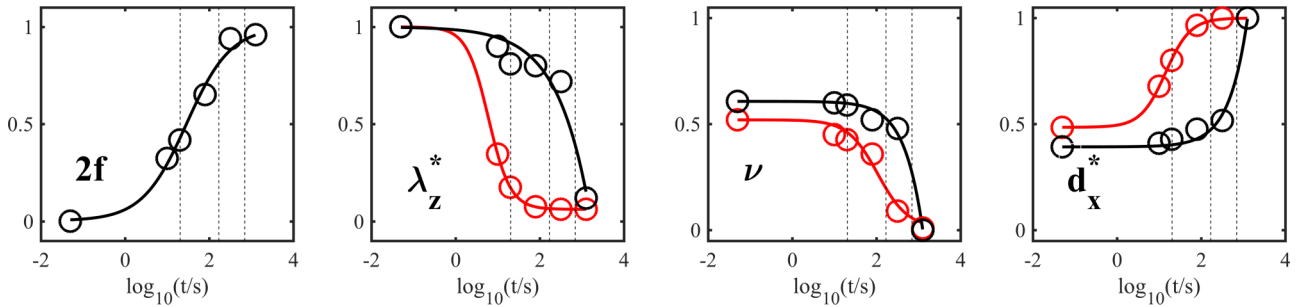


FIG. 3. Time evolution of normalized fit parameters from the DE and WE models: The SiL total dangling end fraction ( $2f$ ), the strain ratio relative to the initial value [ $\lambda_z^* = \lambda_z/\lambda_z(t=0)$ ], the strain coupling parameter ( $\nu$ ), and the derived transverse tube diameter ( $d_x^* = d_x/d_0 = \lambda_x^\nu$  where  $\lambda_x = 1/\sqrt{\lambda_z}$  and  $d_0 = 7.51$  nm). Black data are SiL, red data are SiS. Sigmoidal fits are meant as a guide for the eye. Dashed vertical lines indicate the Rouse and reptation time of the short chains (see Fig. 1), and the 700 s found in Ref. [9] to indicate the end of a rheological transition regime [ $\log(700) \sim 2.85$ ].

213 confirms the  $\nu = 0.5$  nonaffine strain coupling from Ref. [20] 255  
 214 even for the much stronger flow conditions employed here (a 256  
 215 factor  $\sim 15$  higher strain ratio). For  $t > 0$  the fits to the SiS data 257  
 216 predict that at the Rouse time the system is almost relaxed, 258  
 217 and from the effective strain ratio we find that at the 320 s 259  
 218 mark, the system has fully relaxed. For the SiL sample, the 260  
 219 progression of events is clearly different. In the DE model, the 261  
 220 most robust fit parameter is the dangling end fraction, which 262  
 221 effectively weighs the scattering contributions of isotropic and 263  
 222 stretched material. In Fig. 3(a) the evolution of  $f$  shows that 264  
 223 the relaxation of the short chains are delayed in the presence of 265  
 224 the long chains predicting that at  $\tau_{R,S}$  only around 40% of the 266  
 225 short chains have relaxed and that a population of the chains 267  
 226 remain stretched until after  $\tau_{d,S}$  and very close to the 700 s 268  
 227 found to indicate the transition to a pure long chain relaxation 269  
 228 in Ref. [9]. The collective output from the model fits tells the 270  
 229 same story, that the effective strain is felt over a prolonged 271  
 230 time scale in the SiL sample, but the individual fit parameters 272  
 231 provide a much more detailed picture of how the relaxation 273  
 232 progresses. 274

233 In the SiS sample the strain relaxation is almost done after 275  
 234 a Rouse time, while in the SiL sample the strain persist to 276  
 235 times again very close to the 700 s mentioned above; see  $\lambda_z^*$  277  
 236 plot in Fig. 3. Figure 1 shows that the initial relaxation is 278  
 237 faster in the blend than in the pure melt, and in Ref. [9] it 279  
 238 is suggested that the initial fast relaxation is from primarily 280  
 239 stretch relaxation along the chain contour of both short and 281  
 240 long chains. For the short chains we can now attribute this 282  
 241 to the increased stretch, which effectively will excite more 283  
 242 higher relaxation modes. Further, in the SiL sample the derived 284  
 243 transverse tube diameter  $d_x$  remains at a value of roughly 285  
 244  $d_0/2$ , indicating that little transverse relaxation takes place 286  
 245 initially. Thus, the overall structural picture that emerges is that 287  
 246 the rheological transition regime is caused by a cooperative 288  
 247 nematic effect where the short chain stretch and orientation 289  
 248 are maintained by the long chains and relax primarily along 290  
 249 the chains, i.e., by reptation, as already suggested in Ref. [9]. 291  
 250 The long chains relax in this sea of reptating short chains until 292  
 251 around  $t = 700$ s after which they relax in a solvent of relaxed 293  
 252 short chains but likely with a given orientation distribution 294  
 253 which has been collectively maintained during the transition 295  
 254 regime. As mentioned above, we ascribe the increased stretch 296

255 in the blend to direct interactions between the chains. Another 256  
 257 effect of this is manifested in the strain coupling parameter, 258  
 259 which the fits predict to initially be higher than the theoretical 260  
 261 mean field value in the SiL sample. The value of  $\nu_{\text{SiL}} = 0.61$  262  
 263 fits well with values reported for stretched long chain melts 264  
 265 [26] analyzed by Straube *et al.* [27]. There values of 0.63 and 266  
 267 0.57 are reported where the sample has tempered for 60 and 268  
 269 600 s, respectively, after being stretched. There is currently no 269  
 270 theoretical explanation for how such a scaling emerges from 270  
 271 first principles. A final note should be made on the appearance 271  
 272 of lozenges, which in stretched crosslinked network systems 272  
 273 are usually observed as a precursor to the so-called “butterfly” 273  
 274 patterns with the general time progression: ellipses, lozenges, 274  
 275 crosses, butterflies [23]. In our data we see a hint of something 275  
 276 at low  $q$  for the 80 s SiL sample, which could be the onset of a 276  
 277 cross or butterfly pattern but we have no data from 80 to 320 s. 277  
 278 Comparing with similar systems investigated by Hayes *et al.* 278  
 279 [23], it is reasonable for these patterns to appear at this time. 279  
 280 In fact, their appearance validates the use of the DE model for 280  
 281 our noncrosslinked system as it shows that the entanglement 281  
 282 network of the blend is sufficiently sustained over the course 282  
 283 of the measurements. 283

## V. CONCLUSION 277

278 In conclusion, we confirm the ruling out of both nonde- 278  
 279 formed and affinely deformed tubes in entangled melts akin 279  
 280 to crosslinked networks [20]. In the pure short chain melt 280  
 281 we confirm the nonaffine mean-field result  $\nu = 0.5$  for the 281  
 282 strain coupling, even subjecting the sample to a significantly 282  
 283 increased stretch and strain rate than previously documented. 283  
 284 We propose a nonaffine strain coupling relaxation with onset 284  
 285 around the Rouse time of the short chains. In the blend we 285  
 286 demonstrate a nematic field effect on the short chains from the 286  
 287 aligned and stretched long chains showing an initial increased 287  
 288 stretch of the short chains of ca. 50% and a clear nematic effect 288  
 289 influencing the short chain relaxation. The cooperative nematic 289  
 290 effect explains the rheological signature from a structural 290  
 291 perspective, particularly in the intermediate transition regime 291  
 292 appearing after an initial fast stretch-dominated relaxation. 292  
 293 Our data also suggest an increased nonaffine strain coupling 293  
 294 in the blend, which we speculate derives from direct nematic 294

295 interactions not accounted for in current tube theories, and  
 296 as such our structural data will provide input for ongoing  
 297 theoretical efforts implementing direct nematic interactions  
 298 at the fundamental level.

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